



# MACHAKOS UNIVERSITY

University Examinations for 2020/2021

## SCHOOL OF ENGINEERING AND TECHNOLOGY

### DEPARTMENT OF MECHANICAL AND MANUFACTURING ENGINEERING

### FIRST YEAR SECOND SEMESTER EXAMINATION FOR

### BACHELOR OF SCIENCE (ELECTRICAL AND ELECTRONICS ENGINEERING)

### EEE101: ENGINEERING DRAWING AND DESIGN II

DATE: 21/6/2021

TIME: 8:30 – 11:30 AM

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#### INSTRUCTIONS:

1. This paper contains FIVE questions.
2. Answer Question **ONE** and any other **TWO** questions
3. Allow 1½ Hours for question 1 and 45 minutes for each of the other two questions.
4. All dimensions are in millimetres unless otherwise stated.
5. Construction lines should be faint and should not be erased.
6. Accuracy and good line work are essential.

#### QUESTION ONE (COMPULSORY) (30 MARKS)

The part drawings of a Machine Vice are shown in **Figure Q1(a) to (e)**. Assemble the components and draw:

- a) **Sectional view of the assembly**, through the plane X-X as shown in the Figure Q1(a)  
(12 marks)
- b) **Top and End elevation of the assembly**  
(12 marks)
- c) Projection symbol and title block  
(6 marks)

Use first angle projection and do not indicate the dimensions and hidden details.

#### QUESTION TWO (20 MARKS)

**Figure Q2** shows a casting. Draw the sectional view, section XX, and the left side view. Front view is as indicated by the arrow. Indicate the dimensions.

### QUESTION THREE (20 MARKS)

- a) Differentiate between clearance fit and transition fit. (2 marks)
- b) A journal bearing consists of a bronze bush of diameter 130mm fitted into a housing and a steel shaft of 60mm diameter, running in the bush, with oil as a lubricant. Determine the working dimensions of (a) bore of the housing (b) bush and (c) shaft. Calculate the maximum and minimum interference or clearance. Assume interference fit, H7/p6 for the bush and housing and normal running fit, H7/f7 for the shaft and the bush. Refer to Tables 1, 2 and 3. (18 marks)

### QUESTION FOUR (20 MARKS)

Illustrate by using example sketches how the following features are represented in Engineering drawing: Housing, bush, boss, curved slot, rib, fillet, key, keyway, slot and flat.

### QUESTION FIVE (20 MARKS)

- a) Draw a double line sketch of an orthographic pipe network of the single line network shown in **Figure Q5 (a)** (14 marks)
- b) **Figure Q5 (b)** shows Light-sensitive Alarm Project circuit. The circuit detects a sudden shadow falling on the light-sensor and sounds the beeper when this happens. Name **the twelve** devices indicated **1 to 12** in the circuit. (6 marks)

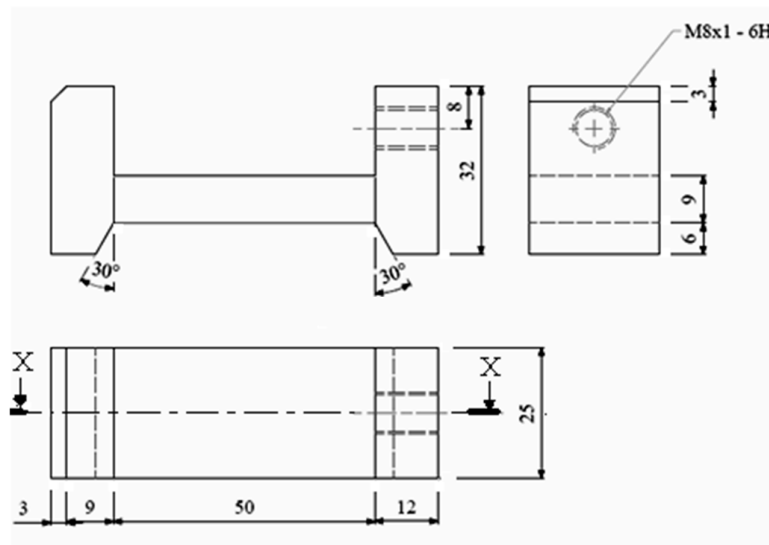
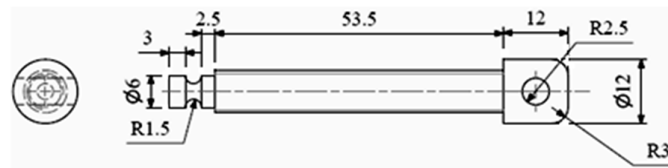
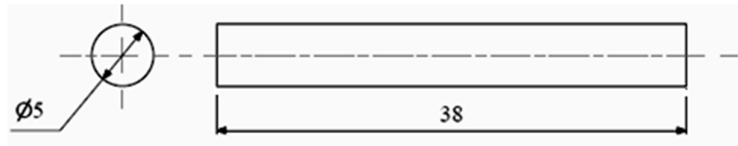


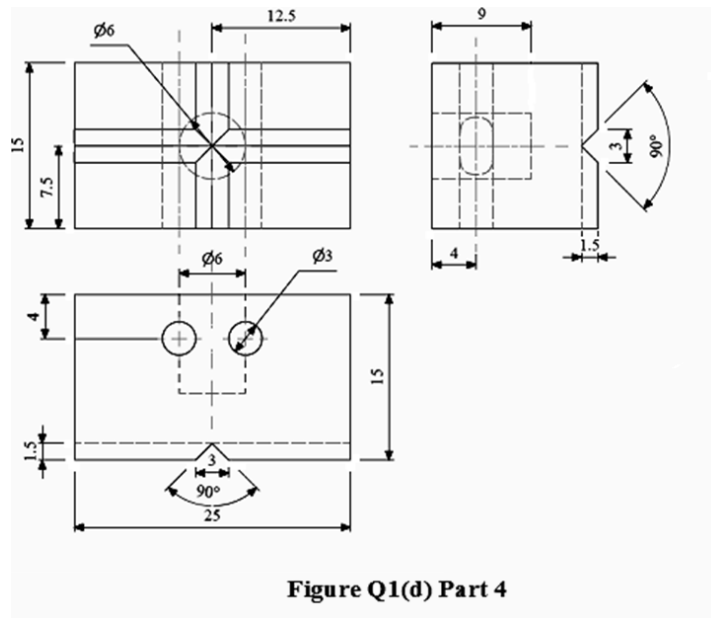
Figure Q1(a) Part 1



**Figure Q1(b) Part 2**



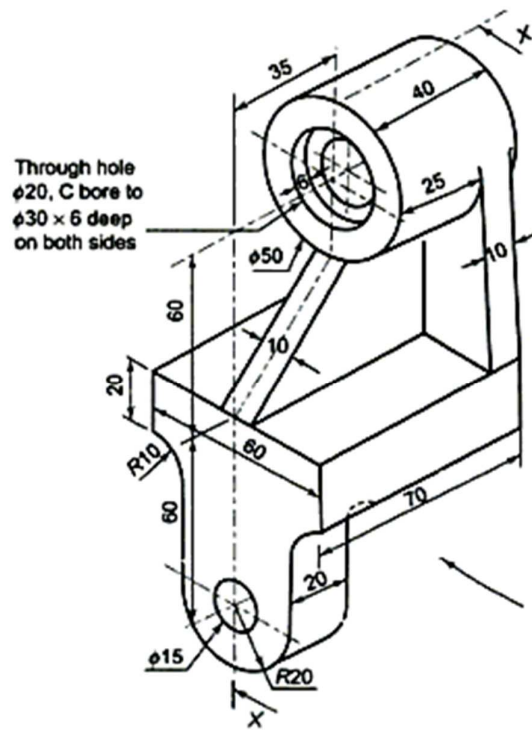
**Figure Q1(c) Part 3**



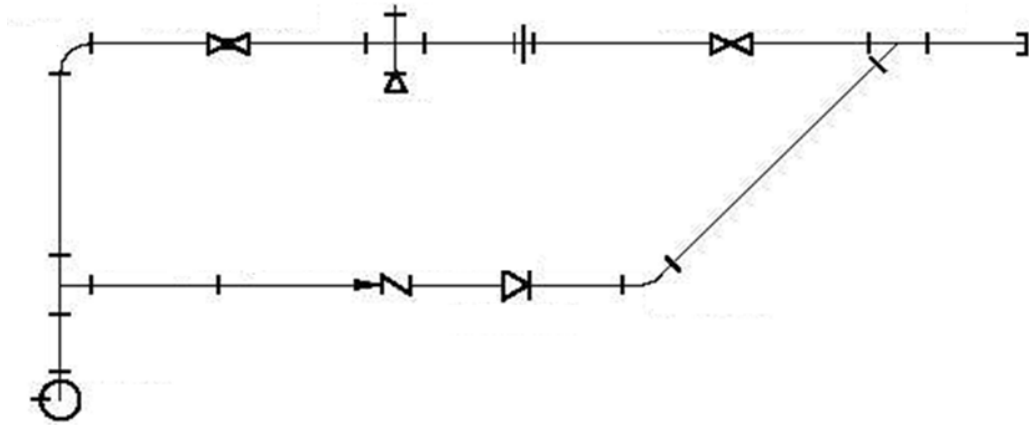
**Figure Q1(d) Part 4**



**Figure Q1(e) Part 5**



**Figure Q2**



**Figure Q5 (a)**

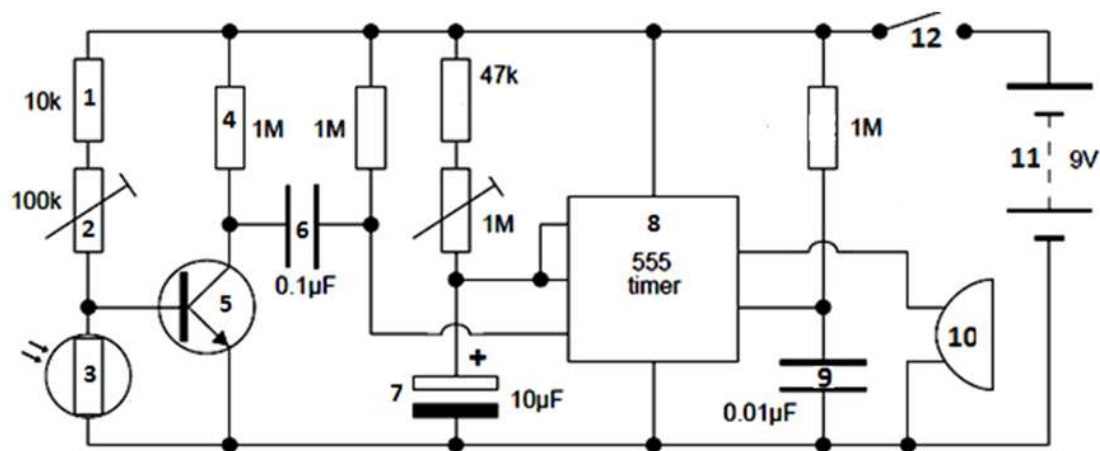


Figure Q5 (b)

Table 1 Fundamental tolerances of grades 01, 0 and 1 to 16 (values of tolerances in microns) (1 micron = 0.001 mm)

| Diameter<br>steps in mm | Tolerance Grades |     |     |     |   |    |    |    |    |    |     |     |     |     |     |      |      |      |
|-------------------------|------------------|-----|-----|-----|---|----|----|----|----|----|-----|-----|-----|-----|-----|------|------|------|
|                         | 01               | 0   | 1   | 2   | 3 | 4  | 5  | 6  | 7  | 8  | 9   | 10  | 11  | 12  | 13  | 14*  | 15*  | 16*  |
| Over 30                 |                  |     |     |     |   |    |    |    |    |    |     |     |     |     |     |      |      |      |
| To and inc 50           | 0.6              | 1   | 1.5 | 2.5 | 4 | 7  | 11 | 16 | 25 | 39 | 62  | 100 | 160 | 250 | 390 | 620  | 1000 | 1600 |
| Over 50                 |                  |     |     |     |   |    |    |    |    |    |     |     |     |     |     |      |      |      |
| To and inc 80           | 0.8              | 1.2 | 2   | 3   | 5 | 8  | 13 | 19 | 30 | 46 | 74  | 120 | 190 | 300 | 460 | 740  | 1200 | 1900 |
| Over 80                 |                  |     |     |     |   |    |    |    |    |    |     |     |     |     |     |      |      |      |
| To and inc 120          | 1                | 1.5 | 2.5 | 4   | 6 | 10 | 15 | 22 | 35 | 54 | 87  | 140 | 220 | 350 | 540 | 870  | 1400 | 2200 |
| Over 120                |                  |     |     |     |   |    |    |    |    |    |     |     |     |     |     |      |      |      |
| To and inc 180          | 1.2              | 2   | 3.5 | 5   | 8 | 12 | 18 | 25 | 40 | 63 | 100 | 160 | 250 | 400 | 630 | 1000 | 1600 | 2500 |

Table 2 Fundamental deviations for shafts of types a to k of sizes upto 500mm (contd.)

| Fundamental deviation in microns |      |                      |       |       |       |      |      |      |   | (1 micron = 0.001 mm) |                      |      |      |        |          |
|----------------------------------|------|----------------------|-------|-------|-------|------|------|------|---|-----------------------|----------------------|------|------|--------|----------|
| Diameter<br>steps in mm          |      | Upper deviation (es) |       |       |       |      |      |      |   | js <sup>+</sup>       | Lower deviation (ei) |      |      |        |          |
|                                  |      | a                    | b     | c     | d     | e    | f    | g    | h |                       | j                    |      |      | k      |          |
| over                             | upto | All grades           |       |       |       |      |      |      |   | ± IT/2                | 5.6                  | 7    | 8    | 4 to 7 | ≤ 3, > 7 |
| 50                               | 65   | − 340                | − 190 | − 140 | − 100 | − 60 | − 30 | − 10 | 0 |                       | − 7                  | − 12 | —    | + 2    | 0        |
| 65                               | 80   | − 360                | − 200 | − 150 |       |      |      |      |   |                       | − 9                  | − 15 | —    | + 3    | 0        |
| 80                               | 100  | − 380                | − 220 | − 170 | − 120 | − 72 | − 36 | − 12 | 0 |                       | − 11                 | − 18 | —    | + 3    | 0        |
| 100                              | 120  | − 410                | − 240 | − 180 |       |      |      |      |   |                       | − 145                | − 85 | − 43 | − 14   | 0        |
| 120                              | 140  | − 460                | − 260 | − 200 | − 145 | − 85 | − 43 | − 14 | 0 |                       | − 11                 | − 18 | —    | + 3    | 0        |
| 140                              | 160  | − 520                | − 280 | − 210 |       |      |      |      |   |                       | − 11                 | − 18 | —    | + 3    | 0        |
| 160                              | 180  | − 580                | − 310 | − 230 |       |      |      |      |   | − 11                  | − 18                 | —    | + 3  | 0      |          |

**Table 2** Fundamental deviations for shafts of types **m** to **zc** of sizes upto 500 mm (*contd.*)

| Fundamental deviation in microns |      |                                |          |          |          |          |          |          |          |          |          |          |           |           | (1 micron = 0.001 mm) |  |
|----------------------------------|------|--------------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|-----------|-----------------------|--|
| Diameter<br>steps in mm          |      | Lower deviations ( <i>ei</i> ) |          |          |          |          |          |          |          |          |          |          |           |           |                       |  |
|                                  |      | <i>m</i>                       | <i>n</i> | <i>p</i> | <i>r</i> | <i>s</i> | <i>t</i> | <i>u</i> | <i>v</i> | <i>x</i> | <i>y</i> | <i>z</i> | <i>za</i> | <i>zb</i> | <i>zc</i>             |  |
| Over                             | Upto | All grades                     |          |          |          |          |          |          |          |          |          |          |           |           |                       |  |
| 30                               | 40   | + 9                            | + 17     | + 26     | + 34     | + 43     | + 48     | + 60     | + 68     | + 80     | + 94     | + 112    | + 148     | + 200     | + 274                 |  |
| 40                               | 50   |                                |          |          |          |          | + 54     | + 70     | + 81     | + 97     | + 114    | + 136    | + 180     | + 242     | + 325                 |  |
| 50                               | 65   | + 11                           | + 20     | + 32     | + 41     | + 53     | + 66     | + 87     | + 102    | + 122    | + 144    | + 172    | + 226     | + 300     | + 405                 |  |
| 65                               | 80   |                                |          |          | + 43     | + 59     | + 75     | + 102    | + 120    | + 146    | + 174    | + 210    | + 274     | + 360     | + 480                 |  |
| 80                               | 100  | + 13                           | + 23     | + 37     | + 51     | + 71     | + 91     | + 124    | + 146    | + 178    | + 214    | + 258    | + 335     | + 445     | + 585                 |  |
| 100                              | 120  |                                |          |          | + 54     | + 79     | + 104    | + 144    | + 172    | + 210    | + 254    | + 310    | + 400     | + 525     | + 690                 |  |
| 120                              | 140  |                                |          |          | + 63     | + 92     | + 122    | + 170    | + 202    | + 248    | + 300    | + 365    | + 470     | + 620     | + 800                 |  |
| 140                              | 160  | + 15                           | + 27     | + 43     | + 65     | + 100    | + 134    | + 190    | + 228    | + 280    | + 340    | + 415    | + 535     | + 700     | + 900                 |  |
| 160                              | 180  |                                |          |          | + 68     | + 108    | + 146    | + 210    | + 252    | + 310    | + 380    | + 465    | + 600     | + 780     | + 1000                |  |

**Table 3** Fundamental deviations for holes of types **A** to **N** for sizes upto 500 mm (*contd.*)

A to N

| Fundamental deviation in microns |      |                       |       |       |       |      |      |      |   |        |      |                       |         | (1 micron = 0.001 mm) |          |                   |          |          |      |                                         |  |  |  |
|----------------------------------|------|-----------------------|-------|-------|-------|------|------|------|---|--------|------|-----------------------|---------|-----------------------|----------|-------------------|----------|----------|------|-----------------------------------------|--|--|--|
| Diameter<br>steps in mm          |      | Lower deviations (EI) |       |       |       |      |      |      |   |        |      | Upper deviations (ES) |         |                       |          |                   |          |          |      |                                         |  |  |  |
|                                  |      | A*                    | %B    | C     | D     | E    | F    | G    | H | Js+    | J    |                       |         | K                     |          | M                 |          | N        |      |                                         |  |  |  |
| Over                             | Upto | All grades            |       |       |       |      |      |      |   | ± IT/2 | 6    | 7                     | 8       | ≤ 8                   | > 8      | ≤ 8 $\frac{1}{2}$ | > 8      | ≤ 8      | > 8* | ≤ 7                                     |  |  |  |
| 30                               | 40   | + 310                 | + 170 | + 120 | + 80  | + 50 | + 25 | + 9  | 0 |        | + 10 | + 14                  | + 24    | - 2 + Δ               | —        | - 9 + Δ           | - 9      | - 17 + Δ | 0    | Same deviation as for<br>grades > 7 + Δ |  |  |  |
| 40                               | 50   | + 320                 | + 180 | + 130 |       |      |      |      |   |        |      |                       |         |                       |          |                   |          |          |      |                                         |  |  |  |
| 50                               | 65   | + 340                 | + 190 | + 140 | + 100 | + 60 | + 30 | + 10 | 0 |        | + 13 | + 18                  | + 28    | - 2 + Δ               | —        | - 11 + Δ          | - 11     | - 20 + Δ | 0    |                                         |  |  |  |
| 65                               | 80   | + 360                 | + 200 | + 150 |       |      |      |      |   |        |      |                       |         |                       |          |                   |          |          |      |                                         |  |  |  |
| 80                               | 100  | + 380                 | + 220 | + 170 | + 120 | + 72 | + 36 | + 12 | 0 | + 16   | + 22 | + 34                  | - 3 + Δ | —                     | - 13 + Δ | - 13              | - 23 + Δ | 0        |      |                                         |  |  |  |
| 100                              | 120  | + 410                 | + 240 | + 180 |       |      |      |      |   |        |      |                       |         |                       |          |                   |          |          |      |                                         |  |  |  |
| 120                              | 140  | + 460                 | + 260 | + 200 | + 145 | + 85 | + 43 | + 14 | 0 |        | + 18 | + 26                  | + 41    | - 3 + Δ               | —        | - 15 + Δ          | - 15     | - 27 + Δ | 0    |                                         |  |  |  |
| 140                              | 160  | + 520                 | + 280 | + 210 |       |      |      |      |   |        |      |                       |         |                       |          |                   |          |          |      |                                         |  |  |  |
| 160                              | 180  | + 580                 | + 310 | + 230 |       |      |      |      |   |        |      |                       |         |                       |          |                   |          |          |      |                                         |  |  |  |